

# Radial Reflection Diffraction Tomography Notes

*S.K. Lehman, S.J. Norton*

**June 27, 2002**

**U.S. Department of Energy**

Lawrence  
Livermore  
National  
Laboratory

## DISCLAIMER

This document was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor the University of California nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or the University of California, and shall not be used for advertising or product endorsement purposes.

This work was performed under the auspices of the U. S. Department of Energy by the University of California, Lawrence Livermore National Laboratory under Contract No. W-7405-Eng-48.

This report has been reproduced directly from the best available copy.

Available electronically at <http://www.doc.gov/bridge>

Available for a processing fee to U.S. Department of Energy

And its contractors in paper from

U.S. Department of Energy

Office of Scientific and Technical Information

P.O. Box 62

Oak Ridge, TN 37831-0062

Telephone: (865) 576-8401

Facsimile: (865) 576-5728

E-mail: [reports@adonis.osti.gov](mailto:reports@adonis.osti.gov)

Available for the sale to the public from

U.S. Department of Commerce

National Technical Information Service

5285 Port Royal Road

Springfield, VA 22161

Telephone: (800) 553-6847

Facsimile: (703) 605-6900

E-mail: [orders@ntis.fedworld.gov](mailto:orders@ntis.fedworld.gov)

Online ordering: <http://www.ntis.gov/ordering.htm>

OR

Lawrence Livermore National Laboratory

Technical Information Department's Digital Library

<http://www.llnl.gov/tid/Library.html>

# Radial Reflection Diffraction Tomography Notes

Sean K. Lehman  
Lawrence Livermore National Laboratory

Steven J. Norton  
Geophex

June 27, 2002

## Abstract

We are developing the theory behind a new imaging modality which uses a single transducer rotating about its center to launch a field radially outward and collect the backscattered (reflected) field. We use diffraction tomography techniques, based upon a linearized version of the field scattering equation, to form images of the medium surrounding the transducer. As there is one transducer which both transmits the incident field and measures the backscattered field, the operation mode is multimonostatic.

## 1 Introduction

Consider a single transducer which rotates about a fixed radius,  $R_0$ , launching pulses at each angular location,  $\theta$ , and measuring the backscattered field. Operating in such a multimonostatic condition, we develop an imaging algorithm based upon a linearized description of the field scattering process. We summarize the operating conditions as follows:

- Transducer rotates at a fixed radius,  $R_0$ , about the origin;
- Must use frequency diversity which implies an incident pulse;
- Multimonostatic reflection operating mode in which the single transducer emits a pulse and records the backscattered field at each angular location,  $\theta$ ;
- Geometry is that of Figure 1.

The transducer is located at  $\mathbf{r}_0 = R_0 (\cos \theta, \sin \theta)$ .

The observation point (to be reconstructed) is located at  $\mathbf{r}' = r' (\cos \theta', \sin \theta')$  where  $R_0 < r'$ .

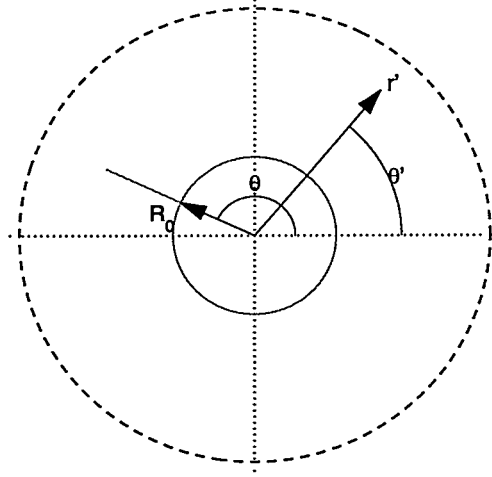


Figure 1: Radial reflection geometry

## 2 Derivation of Forward Model

Use as fundamental equation the Helmholtz equation,

$$[\nabla^2 + k^2(\mathbf{r})] u(\mathbf{r}, \omega) = -p(\mathbf{r}, \omega), \quad (1)$$

where

- $\mathbf{r} \equiv (x, y) = (r, \theta)$  is the spatial coordinate,
- $\omega$  is the temporal frequency,
- $k(\mathbf{r})$  is the wavenumber of the inhomogeneous medium surrounding the transducer,
- $u(\mathbf{r}, \omega)$  is the total field,
- $p(\mathbf{r}, \omega)$  is the incident pulse.

Add  $k_0 u(\mathbf{r}, \omega)$  to both sides of Eqn. 1 where  $k_0 \equiv \omega/v_0$ , and move the inhomogeneous term to the right hand side:

$$[\nabla^2 + k_0^2] u(\mathbf{r}, \omega) = -p(\mathbf{r}, \omega) - [k^2(\mathbf{r}) - k_0^2] u(\mathbf{r}, \omega). \quad (2)$$

Define the *object function* as

$$o(\mathbf{r}) \equiv \frac{k^2(\mathbf{r})}{k_0^2} - 1, \quad (3)$$

and express Eqn. 2 as

$$[\nabla^2 + k_0^2] u(\mathbf{r}, \omega) = -p(\mathbf{r}, \omega) - k_0^2 o(\mathbf{r}) u(\mathbf{r}, \omega). \quad (4)$$

We may use Green's theorem to cast the differential equation of Eqn. 4 into an integral equation,

$$u(\mathbf{r}, \omega) = \int d\mathbf{r}' G(\mathbf{r} - \mathbf{r}', \omega) p(\mathbf{r}', \omega) + k_0^2 \int d\mathbf{r}' G(\mathbf{r} - \mathbf{r}', \omega) o(\mathbf{r}') u(\mathbf{r}'), \quad (5)$$

where we have ignored the boundary conditions and

$$G(\mathbf{r} - \mathbf{r}', \omega) = \frac{e^{ik_0|\mathbf{r}-\mathbf{r}'|}}{4\pi|\mathbf{r} - \mathbf{r}'|}. \quad (6)$$

The *primary source* is

$$u_i(\mathbf{r}, \omega) \equiv \int d\mathbf{r}' G(\mathbf{r} - \mathbf{r}', \omega) p(\mathbf{r}', \omega), \quad (7)$$

so that Eqn. 5 reads

$$u(\mathbf{r}, \omega) = u_i(\mathbf{r}, \omega) + k_0^2 \int d\mathbf{r}' G(\mathbf{r} - \mathbf{r}', \omega) o(\mathbf{r}') u(\mathbf{r}', \omega). \quad (8)$$

The *scattered field* is defined as

$$u_s(\mathbf{r}, \omega) \equiv u(\mathbf{r}, \omega) - u_i(\mathbf{r}, \omega) = k_0^2 \int d\mathbf{r}' G(\mathbf{r} - \mathbf{r}', \omega) o(\mathbf{r}') u(\mathbf{r}', \omega).$$

Evaluate it on the measurement surface,  $r_0 = (R_0, \theta)$ ,

$$u_s(\theta, \omega) = k_0^2 \int d\mathbf{r}' G(\mathbf{r}_0 - \mathbf{r}', \omega) o(\mathbf{r}') u(\mathbf{r}', \omega). \quad (9)$$

Let the incident field be a point source located at  $\mathbf{r}_0$ , obeying

$$[\nabla^2 + k_0^2] u_i(\mathbf{r}, \omega) = -P(\omega) \delta(\mathbf{r}_0 - \mathbf{r}), \quad (10)$$

where  $P(\omega)$  is the incident pulse amplitude. NOTE: Antenna characteristics are not modeled. The incident field is then

$$u_i(\mathbf{r}, \omega) = P(\omega) G(\mathbf{r}_0 - \mathbf{r}, \omega). \quad (11)$$

As is common, invoke the Born approximation,

$$o(\mathbf{r}) \equiv \frac{k^2(\mathbf{r})}{k_0^2} - 1 \approx 0, \quad (12)$$

replace the *total field* by the *incident field*, and express Eqn. 9 as

$$u_s(\theta, \omega) \approx u_s^B(\theta, \omega) \equiv P(\omega) k_0^2 \int d\mathbf{r}' G^2(\mathbf{r}_0 - \mathbf{r}', \omega) o(\mathbf{r}') \quad (13)$$

Eqn. 13 serves as our *forward model*. Express it using Eqn. 6:

$$u_s^B(\theta, \omega) = \frac{P(\omega) k_0^2}{(4\pi)^2} \int d\mathbf{r}' \frac{e^{i2k_0|\mathbf{r}_0-\mathbf{r}'|}}{|\mathbf{r}_0 - \mathbf{r}'|^2} o(\mathbf{r}') \quad (14)$$

Define the *weighted scattered field* as

$$w(\theta, 2\omega) \equiv \frac{4\pi}{P(\omega)k_0^2} u_s^B(\theta, \omega) = \frac{1}{4\pi} \int d\mathbf{r}' \frac{e^{i2k_0|\mathbf{r}_0 - \mathbf{r}'|}}{|\mathbf{r}_0 - \mathbf{r}'|^2} o(\mathbf{r}'). \quad (15)$$

The division by the incident pulse spectrum is equivalent to a deconvolution in the time domain. Thus, this step performs the incident pulse deconvolution of the measured field. A more convenient expression to work with is obtained by differentiating Eqn. 15 by  $k_0$ ,

$$\begin{aligned} \frac{d}{dk_0} w(\theta, 2\omega) &= \frac{1}{4\pi} \int d\mathbf{r}' (i2|\mathbf{r}_0 - \mathbf{r}'|) \frac{e^{i2k_0|\mathbf{r}_0 - \mathbf{r}'|}}{|\mathbf{r}_0 - \mathbf{r}'|^2} o(\mathbf{r}') \\ &= \frac{i2}{4\pi} \int d\mathbf{r}' \frac{e^{i2k_0|\mathbf{r}_0 - \mathbf{r}'|}}{|\mathbf{r}_0 - \mathbf{r}'|} o(\mathbf{r}'), \\ &= i2 \int d\mathbf{r}' G(\mathbf{r}_0 - \mathbf{r}', 2\omega) o(\mathbf{r}'). \end{aligned} \quad (16)$$

Define

$$w'(\theta, 2\omega) \equiv \frac{d}{dk_0} w(\theta, 2\omega) = v_0 \frac{d}{d\omega} w(\theta, 2\omega). \quad (17)$$

We then have

$$-\frac{i}{2} w'(\theta, 2\omega) = \int d\mathbf{r}' G(\mathbf{r}_0 - \mathbf{r}', 2\omega) o(\mathbf{r}'). \quad (18)$$

## 2.1 2.5-D Problem

In cylindrical coordinates, let the measurement surface be at  $\mathbf{r}_0 \equiv (R_0, \theta, z_0)$  for  $R_0$  fixed and  $0 \leq \theta < 2\pi$ . Thus, Eqn. 18 becomes

$$\begin{aligned} -\frac{i}{2} w'(\theta, 2\omega) &= \int_0^\infty r' dr' \int_0^{2\pi} d\theta' \int_{-\infty}^\infty dz' G(\mathbf{r}_0 - \mathbf{r}', 2\omega) o(r', \theta'), \\ &= \int_0^\infty r' dr' \int_0^{2\pi} d\theta' o(r', \theta') \int_{-\infty}^\infty dz' G(\mathbf{r}_0 - \mathbf{r}', 2\omega). \end{aligned} \quad (19)$$

Express  $|\mathbf{r}_0 - \mathbf{r}'|$  in cylindrical coordinates:

$$\begin{aligned} |\mathbf{r}_0 - \mathbf{r}'|^2 &= (x_0 - x')^2 + (y_0 - y')^2 + (z_0 - z')^2 \\ &= (R_0 \cos \theta - r' \cos \theta')^2 + (R_0 \sin \theta - r' \sin \theta')^2 + (z_0 - z')^2 \\ &= R_0^2 + r'^2 - 2R_0 r' \cos(\theta - \theta') + (z_0 - z')^2. \end{aligned} \quad (20)$$

Defining

$$R^2 \equiv R_0^2 + r'^2 - 2R_0 r' \cos(\theta - \theta'), \quad (21)$$

we note that

$$\int_{-\infty}^\infty dz' G(\mathbf{r}_0 - \mathbf{r}', 2\omega) = \frac{i}{4} H_0^{(1)}(2k_0 R).$$

Thus Eqn. 19 reads

$$\begin{aligned} -\frac{i}{2}w'(\theta, 2\omega) &= \frac{i}{4} \int_0^\infty r' dr' \int_0^{2\pi} d\theta' o(r', \theta') H_0^{(1)}(2k_0 R), \\ w'(\theta, 2\omega) &= -\frac{1}{2} \int_0^\infty r' dr' \int_0^{2\pi} d\theta' o(r', \theta') H_0^{(1)}(2k_0 R). \end{aligned} \quad (22)$$

Hankel function expansion from G&R (Eqn.8.530):

$$\boxed{H_0^{(1)}(k_0 R) = \sum_{n=-\infty}^{\infty} J_n(k_0 R_0) H_n^{(1)}(k_0 r') e^{in(\theta-\theta')}} \quad (23)$$

where  $R_0 < r'$ . Substituting this into Eqn. 22 yields

$$w'(\theta, 2\omega) = -\frac{1}{2} \sum_{n=-\infty}^{\infty} \int_0^\infty r' dr' \int_0^{2\pi} d\theta' o(r', \theta') J_n(2k_0 R_0) H_n^{(1)}(2k_0 r') e^{in(\theta-\theta')} \quad (24)$$

Fourier expand the object and weighted measured field functions as follows:

$$o_n(r') = \frac{1}{2\pi} \int_0^{2\pi} d\theta' o(r', \theta') e^{-in\theta'}, \quad (25)$$

$$o(r', \theta') = \sum_{n=-\infty}^{\infty} o_n(r') e^{in\theta'}. \quad (26)$$

and

$$w'_n(2\omega) = \frac{1}{2\pi} \int_0^{2\pi} d\theta w(\theta, 2\omega) e^{-in\theta}, \quad (27)$$

$$w'(\theta, 2\omega) = \sum_{n=-\infty}^{\infty} w'_n(2\omega) e^{in\theta}. \quad (28)$$

Using Eqn. 27 to transform Eqn. 24, yields

$$\begin{aligned} \frac{1}{2\pi} \int_0^{2\pi} d\theta w'(\theta, 2\omega) e^{-im\theta} &= -\frac{1}{4\pi} \sum_{n=-\infty}^{\infty} J_n(2k_0 R_0) \int_0^\infty r' dr' H_n^{(1)}(2k_0 r') \times \\ &\quad \underbrace{\int_0^{2\pi} d\theta' o(r', \theta') e^{-in\theta'}}_{\equiv 2\pi o_n(r')} \underbrace{\int_0^{2\pi} d\theta e^{i(n-m)\theta}}_{\equiv 2\pi \delta_{mn}} \end{aligned} \quad (29)$$

Using Eqn. 25 and

$$\frac{1}{2\pi} \int_0^{2\pi} d\theta e^{i(m-n)\theta} = \delta_{mn}$$

reduces Eqn. 29 to

$$w'_m(2\omega) = -\pi J_m(2k_0 R_0) \int_0^\infty r' dr' H_m^{(1)}(2k_0 r') o_m(r'). \quad (30)$$

Define the Bessel function normalized field derivative as

$$v'_m(2\omega) \equiv -\frac{1}{\pi J_m(2k_0 R_0)} w'_m(2\omega) = -\frac{4v_0^3}{J_m(2k_0 R_0)} \frac{d}{d\omega} \left[ \frac{u_m(\omega)}{P(\omega)\omega^2} \right], \quad (31)$$

where we have used Eqns. 15 and 17, and express Eqn. 30 as

$$v'_m(2\omega) = \int_0^\infty r' dr' H_m^{(1)}(2k_0 r') o_m(r'). \quad (32)$$

If we assume the object function,  $o(r, \theta)$ , is real, we have from Eqn. 25 that

$$o_{-m}^*(r') = o_m(r').$$

Using this and the property of Hankel functions,

$$(-1)^m H_{-m}^{(1)}(2k_0 r) = H_m^{(1)}(2k_0 r),$$

we may solve for  $o_m(r)$ . Define

$$\begin{aligned} P_m(2\omega) &= v'_m(2\omega) + (-1)^m v_{-m}'^*(2\omega), \\ &= \int_0^\infty r' dr' H_m^{(1)}(2k_0 r') o_m(r') + \int_0^\infty r' dr' (-1)^m H_{-m}^{(1)*}(2k_0 r') o_{-m}^*(r'), \\ &= \int_0^\infty r' dr' [H_m^{(1)}(2k_0 r') + H_m^{(1)*}(2k_0 r')] o_m(r'), \\ &= 2 \int_0^\infty r' dr' J_m(2k_0 r') o_m(r'). \end{aligned} \quad (33)$$

Eqn. 33 is proportional to the Bessel transform of the object,

$$o_m(2k_0) \equiv \int_0^\infty r' dr' J_m(2k_0 r') o_m(r'), \quad (34)$$

so, we may express it as

$$o_m(2k_0) = \frac{1}{2} P_m(2\omega). \quad (35)$$

Explicitly expressing Eqn. 35 in terms of the measured field, we find

$$\begin{aligned} P_m(2\omega) &= v'_m(2\omega) + (-1)^m v_{-m}'^*(2\omega), \\ &= -4v_0^3 \left[ \frac{1}{J_m(2k_0 R_0)} \frac{d}{d\omega} \left[ \frac{u_m(\omega)}{P(\omega)\omega^2} \right] + \frac{(-1)^m}{J_{-m}(2k_0 R_0)} \left( \frac{d}{d\omega} \left[ \frac{u_{-m}(\omega)}{P(\omega)\omega^2} \right] \right)^* \right], \\ &= -\frac{4v_0^3}{J_m(2k_0 R_0)} \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right]. \end{aligned} \quad (36)$$



Substituting Eqn. 36 into Eqn. 35, we find the “Fourier-Bessel Diffraction Theorem” for RRDT:

$$o_m(2k_0) = -\frac{2v_0^3}{J_m(2k_0R_0)} \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right]. \quad (37)$$

Using the orthogonality of Bessel functions, consider the following integral

$$I = \int_0^\infty k dk J_m(kr) J_m(kr') = \frac{1}{r} \delta(r - r'),$$

we may invert this equation for  $o_m(r)$ :

$$\begin{aligned} 4 \int_0^\infty k_0 dk_0 P_m(2k_0v_0) J_m(2k_0r) &= 8 \int_0^\infty k_0 dk_0 \int_0^\infty r' dr' J_m(2k_0r') J_m(2k_0r) o_m(r'), \\ &= 8 \int_0^\infty r' dr' \int_0^\infty k_0 dk_0 J_m(2k_0r') J_m(2k_0r) o_m(r'), \\ &= 8 \int_0^\infty r' dr' \frac{1}{r'} \delta(r - r') o_m(r'), \\ &= 8 o_m(r). \end{aligned}$$

$$o_m(r) = 2 \int_0^\infty k_0 dk_0 P_m(2k_0) J_m(2k_0r). \quad (38)$$

Substituting this into Eqn. 26 yields the reconstruction:

$$o(r, \theta) = \sum_{m=-\infty}^{\infty} e^{im\theta} \int_0^\infty k_0 dk_0 P_m(2k_0) J_m(2k_0r). \quad (39)$$

Substitute Eqn. 36 into Eqn. 39:

$$\begin{aligned} o(r, \theta) &= -8v_0^3 \sum_{m=-\infty}^{\infty} e^{im\theta} \int_0^\infty k_0 dk_0 \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right] \frac{J_m(2k_0r)}{J_m(2k_0R_0)}, \\ &= -8v_0 \sum_{m=-\infty}^{\infty} e^{im\theta} \int_0^\infty \omega d\omega \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right] \frac{J_m(2k_0r)}{J_m(2k_0R_0)}. \end{aligned} \quad (40)$$

For later on, define the integral in Eqn. 40 as

$$I_m(r) \equiv \int_0^\infty \omega d\omega \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right] \frac{J_m(2k_0r)}{J_m(2k_0R_0)}, \quad (41)$$

and express Eqn. 40 as

$$o(r, \theta) = -8v_0^3 \sum_{m=-\infty}^{\infty} I_m(r) e^{im\theta}. \quad (42)$$

We must now consider how to perform numerically the integral in Eqn. 41. There is a potential problem with the  $J_m^{-1}(2k_0R_0)$  term which contains an infinite number of zeros along the real axis.

## 2.2 Extend the Integral of Eqn. 41 over the Entire Real Axis

First some observations. The Fourier transform of the pulse is

$$P(\omega) = \int_0^\infty dt p(t) e^{i\omega t},$$

thus for a real pulse, we have

$$P(-\omega) = P^*(\omega). \quad (43)$$

The polar Fourier transform of the measured field is

$$u_m(\omega) = \frac{1}{2\pi} \int_0^{2\pi} d\theta \int_0^\infty dt u(\theta, t) e^{i\omega t} e^{-im\theta},$$

thus we have

$$u_m(-\omega) = u_{-m}^*(\omega). \quad (44)$$

Using these identities, we may express  $I_m(r)$  as

$$I_m(r) = \int_{-\infty}^0 \omega d\omega \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right] \frac{J_m(2k_0 r)}{J_m(2k_0 R_0)}. \quad (45)$$

Adding Eqns 41 and 45, we have

$$I_m(r) = \frac{1}{2} \int_{-\infty}^\infty \omega d\omega \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right] \frac{J_m(2k_0 r)}{J_m(2k_0 R_0)}, \quad (46)$$

which has extended the integral over the entire real axis.

## 2.3 Performing the Integral of Eqn. 46

The difficulty in integrating Eqn. 46 is the reciprocal of the Bessel function,  $J_m(2k_0 R_0)$ , which has multiple zeros along the real axis. We circumvent this issue by continuing the integral into the complex  $\omega$ -plane and performing a contour integration. Care must be taken, however, since  $J_m(2k_0 r)$  diverges in both the upper and lower half planes requiring us to express it as

$$J_m(2k_0 r) = \frac{1}{2} [H_m^{(1)}(2k_0 r) + H_m^{(2)}(2k_0 r)]. \quad (47)$$

and separating the integral into two. The one containing  $H_m^{(1)}(2k_0 r)$  is closed in the upper half plane, whereas the one containing  $H_m^{(2)}(2k_0 r)$  is closed in the lower half plane. We have

$$I_m(r) = \frac{1}{4} \int_{C^+} \omega d\omega \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right] \frac{H_m^{(1)}(2k_0 r)}{J_m(2k_0 R_0)} + \frac{1}{4} \int_{C^-} \omega d\omega \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right] \frac{H_m^{(2)}(2k_0 r)}{J_m(2k_0 R_0)}, \quad (48)$$

where the  $C^+$  contour is closed in the upper half plane, and the  $C^-$  contour is closed in the lower half plane. The  $C^+$  contour excludes the real  $\omega < 0$  poles but includes the real  $\omega > 0$  poles. The  $C^-$  contour is the opposite. These are shown in Figure 2.

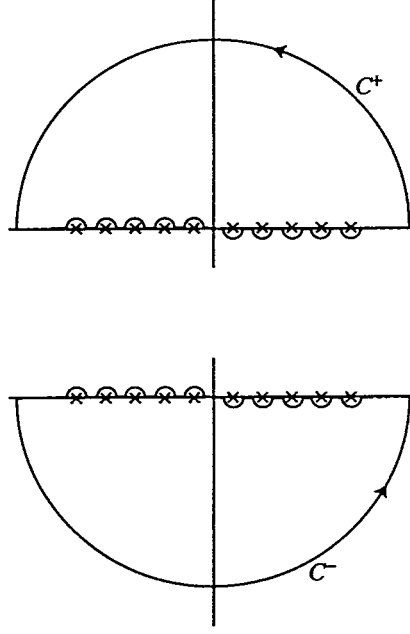


Figure 2: *Integration contours.*

## 2.4 The Residues at the zeros of $J_m(2k_0 R_0)$

In anticipation of requiring the residues of  $1/J_m(2k_0 R_0)$  at the zeros of the Bessel function, we compute them as follows,

$$\begin{aligned}
 j_{mn} &= \text{Res}_{z \rightarrow \alpha_{mn}} \left\{ \frac{1}{J_m(z)} \right\} = \lim_{z \rightarrow \alpha_{mn}} \frac{z - \alpha_{mn}}{J_m(z)}, \\
 &= \lim_{z \rightarrow \alpha_{mn}} \frac{2}{J_{m-1}(z) - J_{m+1}(z)}, \quad (\text{L'Hôpital's Rule}) \\
 &= \frac{2}{J_{m-1}(\alpha_{mn}) - J_{m+1}(\alpha_{mn})}, \quad (49)
 \end{aligned}$$

where  $\alpha_{mn}$  is the  $n^{\text{th}}$  zero of the  $m^{\text{th}}$  Bessel function, and  $j_{mn}$  is the residue at the positive pole. For negative poles, we have

$$\begin{aligned}
 k_{mn} &= \text{Res}_{z \rightarrow -\alpha_{mn}} \left\{ \frac{1}{J_m(z)} \right\} = \lim_{z \rightarrow -\alpha_{mn}} \frac{z + \alpha_{mn}}{J_m(z)}, \\
 &= \lim_{z \rightarrow -\alpha_{mn}} \frac{2}{J_{m-1}(z) - J_{m+1}(z)}, \quad (\text{L'Hôpital's Rule}) \\
 &= \frac{2}{J_{m-1}(-\alpha_{mn}) - J_{m+1}(-\alpha_{mn})}. \quad (50)
 \end{aligned}$$

Use  $J_m(-z) = (-1)^m J_m(z)$  to find the  $k_{mn}$  and  $j_{mn}$  are related via

$$\begin{aligned}
k_{mn} &= \frac{2}{(-1)^{m-1} J_{m-1}(\alpha_{mn}) - (-1)^{m+1} J_{m+1}(\alpha_{mn})}, \\
&= \frac{(-1)^{m+1} 2}{J_{m-1}(\alpha_{mn}) - J_{m+1}(\alpha_{mn})}, \\
&= (-1)^{m+1} j_{mn}.
\end{aligned} \tag{51}$$

## 2.5 Perform Complex Integration

Replace the contour integrals of Eqn. 48 by the sum of the residues,

$$\begin{aligned}
I_m(r) &= i\pi \sum_{n=1}^{\infty} \text{Res}_{2k_0 R_0 \rightarrow \alpha_{mn}} \left\{ \omega \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right] \frac{H_m^{(1)}(2k_0 r)}{J_m(2k_0 R_0)} \right\} \\
&\quad - \frac{i\pi}{2} \sum_{n=1}^{\infty} \text{Res}_{2k_0 R_0 \rightarrow -\alpha_{mn}} \left\{ \omega \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right] \frac{H_m^{(1)}(2k_0 r)}{J_m(2k_0 R_0)} \right\} \\
&\quad - \frac{i\pi}{2} \sum_{n=1}^{\infty} \text{Res}_{2k_0 R_0 \rightarrow \alpha_{mn}} \left\{ \omega \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right] \frac{H_m^{(2)}(2k_0 r)}{J_m(2k_0 R_0)} \right\} \\
&\quad + i\pi \sum_{n=1}^{\infty} \text{Res}_{2k_0 R_0 \rightarrow -\alpha_{mn}} \left\{ \omega \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right] \frac{H_m^{(2)}(2k_0 r)}{J_m(2k_0 R_0)} \right\}
\end{aligned} \tag{52}$$

Note

$$\begin{aligned}
2k_0 R_0 \rightarrow \alpha_{mn} &\Rightarrow k_0 = \frac{\alpha_{mn}}{2R_0} \quad \text{and} \quad \omega = \frac{\alpha_{mn} v_0}{2R_0}, \\
2k_0 R_0 \rightarrow -\alpha_{mn} &\Rightarrow k_0 = -\frac{\alpha_{mn}}{2R_0} \quad \text{and} \quad \omega = -\frac{\alpha_{mn} v_0}{2R_0}.
\end{aligned} \tag{53}$$

Define

$$\omega_{mn} \equiv \frac{\alpha_{mn} v_0}{2R_0}, \tag{54}$$

$$\hat{r} \equiv \frac{r}{R_0}, \tag{55}$$

$$A_m(\omega) \equiv \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right]. \tag{56}$$

Substitute Eqns. 49 and 51 into Eqn. 52 and use the above definitions,

$$\begin{aligned}
I_m(r) = & i\pi \sum_{n=1}^{\infty} j_{mn} \omega_{mn} A_m(\omega_{mn}) H_m^{(1)}(\alpha_{mn} \hat{r}) \\
& - \frac{i\pi}{2} \sum_{n=1}^{\infty} (-1)^{m+1} j_{mn} \omega_{mn} A_m(-\omega_{mn}) H_m^{(1)}(-\alpha_{mn} \hat{r}) \\
& - \frac{i\pi}{2} \sum_{n=1}^{\infty} j_{mn} \omega_{mn} A_m(\omega_{mn}) H_m^{(2)}(\alpha_{mn} \hat{r}) \\
& + i\pi \sum_{n=1}^{\infty} (-1)^{m+1} j_{mn} \omega_{mn} A_m(-\omega_{mn}) H_m^{(2)}(-\alpha_{mn} \hat{r})
\end{aligned} \tag{57}$$

Note, using  $H_m^{(1,2)}(-z) = (-1)^m H_m^{(1,2)}(z)$ , we have

$$(-1)^{m+1} H_m^{(1,2)}(-z) = (-1)^{2m+1} H_m^{(1,2)}(z) = -H_m^{(1,2)}(z).$$

So we have

$$\begin{aligned}
I_m(r) = & i\pi \sum_{n=1}^{\infty} j_{mn} \omega_{mn} A_m(\omega_{mn}) H_m^{(1)}(\alpha_{mn} \hat{r}) \\
& + \frac{i\pi}{2} \sum_{n=1}^{\infty} j_{mn} \omega_{mn} A_m(-\omega_{mn}) H_m^{(1)}(\alpha_{mn} \hat{r}) \\
& - \frac{i\pi}{2} \sum_{n=1}^{\infty} j_{mn} \omega_{mn} A_m(\omega_{mn}) H_m^{(2)}(\alpha_{mn} \hat{r}) \\
& - i\pi \sum_{n=1}^{\infty} j_{mn} \omega_{mn} A_m(-\omega_{mn}) H_m^{(2)}(\alpha_{mn} \hat{r}), \\
= & i\pi \sum_{n=1}^{\infty} j_{mn} \omega_{mn} \left( A_m(\omega_{mn}) + \frac{1}{2} A_m(-\omega_{mn}) \right) H_m^{(1)}(\alpha_{mn} \hat{r}) \\
& - \left( \frac{1}{2} A_m(\omega_{mn}) + A_m(-\omega_{mn}) \right) H_m^{(2)}(\alpha_{mn} \hat{r}), \\
= & \frac{i\pi}{2} \sum_{n=1}^{\infty} j_{mn} \omega_{mn} \left[ \left( A_m(\omega_{mn}) - A_m(-\omega_{mn}) \right) J_m(\alpha_{mn} \hat{r}) \right. \\
& \left. + 3i \left( A_m(\omega_{mn}) + A_m(-\omega_{mn}) \right) N_m(\alpha_{mn} \hat{r}) \right].
\end{aligned} \tag{58}$$

Finally, we note that  $P(\omega)$  and  $u_m(\omega)$  are band limited to  $\omega \in [\omega_{\min}, \omega_{\max}] \equiv \Omega$ .

$$\begin{aligned}
I_m(r) = & \frac{i\pi}{2} \sum_{\alpha_{mn} \in \Omega} j_{mn} \omega_{mn} \left[ \left( A_m(\omega_{mn}) - A_m(-\omega_{mn}) \right) J_m(\alpha_{mn} \hat{r}) \right. \\
& \left. + 3i \left( A_m(\omega_{mn}) + A_m(-\omega_{mn}) \right) N_m(\alpha_{mn} \hat{r}) \right].
\end{aligned} \tag{59}$$

Substituting Eqn. 57 back into Eqn. 40, we have the final form for the reconstruction

$$o(r, \theta) = -4i\pi v_0 \sum_{m=-\infty}^{\infty} e^{im\theta} \sum_{\alpha_{mn} \in \Omega} j_{mn} \omega_{mn} \left[ \left( A_m(\omega_{mn}) - A_m(-\omega_{mn}) \right) J_m(\alpha_{mn} \hat{r}) + 3i \left( A_m(\omega_{mn}) + A_m(-\omega_{mn}) \right) N_m(\alpha_{mn} \hat{r}) \right]. \quad (60)$$

### 3 Sanity Check: Test Reconstruction with a Symmetric Object

The object is independent of angle,

$$o(r, \theta) \equiv o(r).$$

Then the polar transform of the field is

$$u_m(\omega) = \frac{1}{2\pi} \int_0^{2\pi} d\theta u(\omega) e^{-im\theta} = u(\omega) \delta_{m0}.$$

Then Eqn. 60 reduces to

$$o(r) = -4i\pi v_0 \sum_{\alpha_{0n} \in \Omega} j_{0n} \omega_{0n} \left[ \left( A_0(\omega_{0n}) - A_0(-\omega_{0n}) \right) J_0(\alpha_{0n} \hat{r}) + 3i \left( A_0(\omega_{0n}) + A_0(-\omega_{0n}) \right) N_0(\alpha_{0n} \hat{r}) \right]. \quad (61)$$

Note,

$$A_0(\pm\omega_{0n}) \equiv \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u(\omega)}{P(\omega)} + \frac{u^*(\omega)}{P^*(\omega)} \right) \right]_{\omega=\pm\omega_{0n}} = 2 \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \text{Re} \left\{ \frac{u(\omega)}{P(\omega)} \right\} \right]_{\omega=\pm\omega_{0n}}. \quad (62)$$

Using the symmetry properties of Eqns. 43 and 44, we find

$$A_0(\omega_{0n}) - A_0(-\omega_{0n}) = 0,$$

which reduces the reconstruction to

$$o(r) = \frac{48\pi v_0^2}{R_0} \sum_{\alpha_{0n} \in \Omega} \frac{\alpha_{0n} N_0 \left( \alpha_{0n} \frac{r}{R_0} \right)}{J_{-1}(\alpha_{0n}) - J_1(\alpha_{0n})} \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \text{Re} \left\{ \frac{u(\omega)}{P(\omega)} \right\} \right]_{\omega=\omega_{0n}}, \quad (63)$$

where we have substituted,

$$\omega_{0n} = \frac{\alpha_{0n} v_0}{2R_0}, \quad (64)$$

$$\hat{r} = \frac{r}{R_0}, \quad (65)$$

$$j_{0n} = \frac{2}{J_{-1}(\alpha_{0n}) - J_1(\alpha_{0n})}. \quad (66)$$

**The reconstruction is pure real.**

## 4 Fourier & Fourier-Bessel Transforms, & Fourier Diffraction Theorem

The derivations used herein are based upon the Fourier-Bessel transform pair:

$$F_m(k) = \frac{1}{2\pi} \int_0^{2\pi} d\theta \int_0^\infty r dr f(r, \theta) e^{-im\theta} J_m(kr), \quad (67)$$

$$f(r, \theta) = \sum_{m=-\infty}^{\infty} \int_0^\infty k dk F_m(k) e^{im\theta} J_m(kr) \quad (68)$$

The Cartesian Fourier transform pair,

$$F(k_x, k_y) = \int_{-\infty}^{\infty} dx \int_{-\infty}^{\infty} dy F(x, y) e^{-i(k_x x + k_y y)},$$

$$f(x, y) = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} dk_x \int_{-\infty}^{\infty} dk_y F(k_x, k_y) e^{i(k_x x + k_y y)},$$

can be cast into polar coordinates using the following change of variables,

$x = r \cos \theta,$	$k_x = k \cos \phi,$
$y = r \sin \theta,$	$k_y = k \sin \phi,$

to yield

$$F(k, \phi) = \int_0^{2\pi} d\theta \int_0^\infty r dr f(r, \theta) e^{-ikr \cos(\theta - \phi)}, \quad (69)$$

$$f(r, \theta) = \frac{1}{(2\pi)^2} \int_0^{2\pi} d\phi \int_0^\infty k dk F(k, \phi) e^{ikr \cos(\theta - \phi)}. \quad (70)$$

To determine the relationship between  $F(k, \phi)$  and  $F_m(k)$ , substitute the expansion

$$e^{-ikr \cos \theta} = \sum_{m=-\infty}^{\infty} (-i)^m J_m(kr) e^{im\theta}$$

into Eqn. 69

$$\begin{aligned} F(k, \phi) &= \int_0^{2\pi} d\theta \int_0^\infty r dr f(r, \theta) \left[ \sum_{m=-\infty}^{\infty} (-i)^m J_m(kr) e^{im(\phi - \theta)} \right], \\ &= \sum_{m=-\infty}^{\infty} (-i)^m e^{im\phi} \int_0^{2\pi} d\theta \int_0^\infty r dr f(r, \theta) J_m(kr) e^{-im\theta} \\ &= \sum_{m=-\infty}^{\infty} (-i)^m e^{im\phi} F_m(k). \end{aligned} \quad (71)$$

Using  $\frac{1}{2\pi} \int_0^{2\pi} d\theta e^{i(m-n)\theta} = \delta_{mn}$ , we may invert Eqn. 71 to find

$$F_m(k) = \frac{(-i)^{-m}}{2\pi} \int_0^{2\pi} d\phi F(k, \phi) e^{-im\phi}. \quad (72)$$

#### 4.1 The RRDT Fourier Diffraction Theorem

Substitute Eqn. 37 into Eqn. 71 to obtain the Fourier Diffraction Theorem for RRDT,

$$\begin{aligned} O(2k_0, \phi) &= \sum_{m=-\infty}^{\infty} (-i)^m e^{im\phi} o_m(2k_0), \\ &= -2v_0^3 \sum_{m=-\infty}^{\infty} \frac{(-i)^m e^{im\phi}}{J_m(2k_0 R_0)} \frac{d}{d\omega} \left[ \frac{1}{\omega^2} \left( \frac{u_m(\omega)}{P(\omega)} + \frac{u_{-m}^*(\omega)}{P^*(\omega)} \right) \right]. \end{aligned} \quad (73)$$

This is shown graphically in Figure 3.



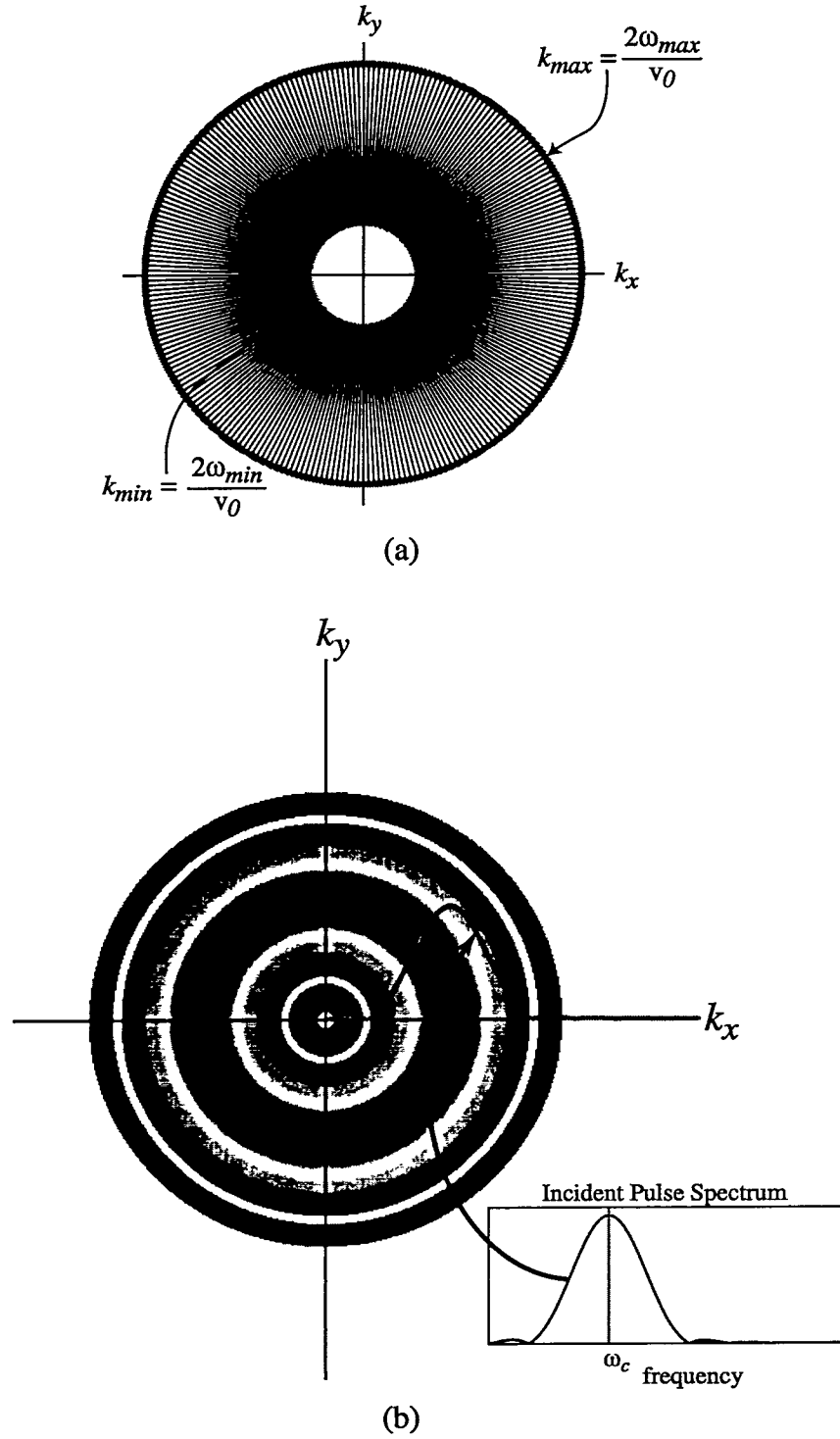


Figure 3: *Radial reflection Fourier diffraction theorem.*